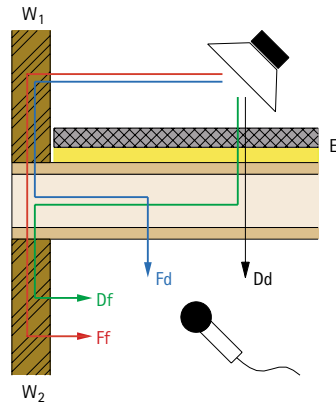




Prognosis of airborne sound transmission in separating floors



$W_1 + W_2$	5	6
1	$R_{Ff,w,R} = 72\text{dB}$ $R_{Fd,w,R} = 82\text{dB}$ $R_{Df,w,R} \sim 85\text{dB}$	$R_{Ff,w,R} = 72\text{dB}$ $R_{Fd,w,R} = 70\text{dB}$ $R_{Df,w,R} \sim 85\text{dB}$
2		
3	$R_{Ff,w,R} = 70\text{dB}$ $R_{Fd,w,R} = 80\text{dB}$ $R_{Df,w,R} \sim 85\text{dB}$	$R_{Ff,w,R} = 70\text{dB}$ $R_{Fd,w,R} = 67\text{dB}$ $R_{Df,w,R} \sim 85\text{dB}$
4	$R_{Ff,w,R} = 64\text{dB}$ $R_{Fd,w,R} = 80\text{dB}$ $R_{Df,w,R} \sim 85\text{dB}$	$R_{Ff,w,R} = 64\text{dB}$ $R_{Fd,w,R} = 63\text{dB}$ $R_{Df,w,R} \sim 85\text{dB}$

The forecast model for airborne noise insulation in buildings essentially corresponds to DIN EN 12354-1. Calculating the noise insulation R' including all flanking transmissions is done based on the following equation.

$$R'_w = -10 \log \left(10^{-\frac{R_w}{10}} + \sum_{ij=1}^n 10^{-\frac{R_{ij,w}}{10}} \right) \text{ dB}$$

$$R_{ij,w} = R_{ij,w,R} + 10 \log \frac{l_{lab}}{l_{Bau}} + 10 \log \frac{S_S}{A_0} \text{ dB}$$

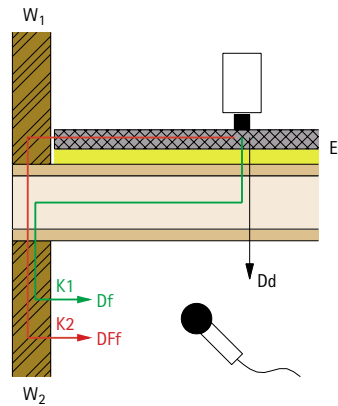
- R_w evaluated noise reduction index of the separating floor without flanking transmission
- $R_{ij,w}$ evaluated flanking reduction index for flanking transmission paths ij in the building
- $R_{ij,w,R}$ calculated value of the evaluated flanking reduction index for flanking transmission paths ij with edge lengths of l_{lab}
- n number of walls
- l_{lab} edge length between the separating component and the flanking component in the laboratory
- l_{Bau} edge length between the separating component and the flanking component in the building
- S_S separating surface in the building
- A_0 reference absorption surface, $A_0 = 10\text{m}^2$
- W_1 wall structure of transmitting room
- W_2 wall structure of receiving room

- E screed
- 1 gypsum fibreboard (GF) or plasterboard (GKB)
- 2 cross laminated timber (CLT) and GF or GKB (level of installation $d \geq 60\text{mm}$)
- 3 composite board
- 4 cross laminated timber (CLT)
- 5 LIGNATUR with suspended ceiling
- 6 LIGNATUR

Part of the basic data for the forecast has been taken from the new component catalogue of DIN 4109. We have performed a large number of measurements with respect to this method for LIGNATUR silence12.



Prognosis of impact sound transmission in separating floors



K_1 (dB)		5		6	
W_2					
1	2	7		1	
3	4	9		4	

K_2 (dB)		$L_{n,w} + K_1$ (dB)															
$W_1 + W_2$	E	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53
1	7	4	4	3	3	2	2	1	1	1	1	1	1	0	0	0	0
	8	3	3	2	2	1	1	1	1	1	1	0	0	0	0	0	0
3	7	8	7	6	5	5	4	4	3	3	2	2	1	1	1	1	1
	8	5	5	4	4	3	3	2	2	1	1	1	1	1	1	0	0

We developed the forecast model for impact sound transmission in cooperation with the ift Rosenheim following DIN EN 12354-2.

The standard impact sound level in buildings is composed of the direct impact sound transmission L_n of the floor and the flanking walls. The transmission values relevant in timber constructions are shown in the diagram on the left.

The shares of flanking transmissions $L_{n,Df}$ and $L_{n,Dff}$ correspond to the sum of the sound transmissions via all four flanking walls.

For impact sound calculation the shares of the transmission paths from the above equation were converted into correction summands.

$$L'_{n,w} = L_{n,w} + K_1 + K_2$$

$L_{n,w}$ evaluated standard impact sound level of the separating floor without flanking transmission

K_1 correction summand for transmission via path Df

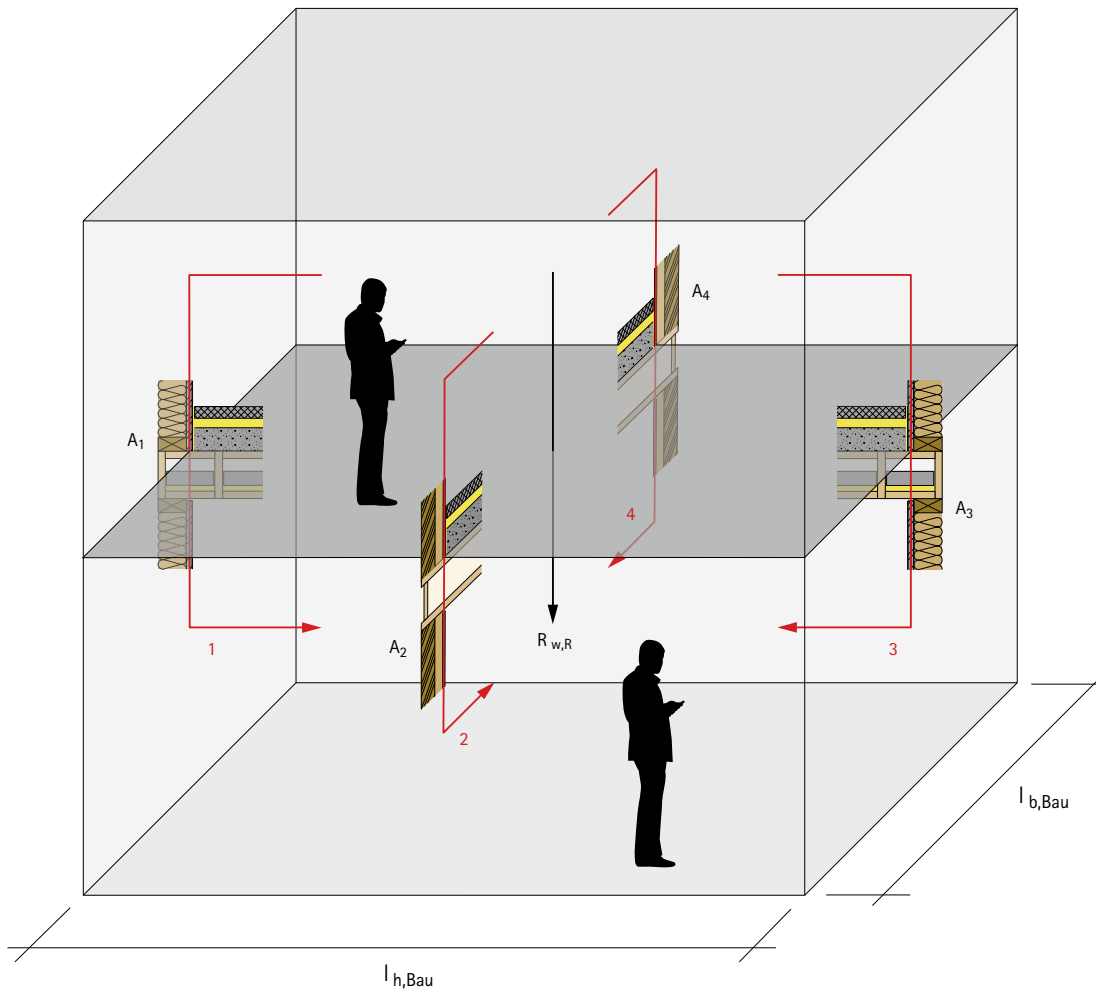
K_2 correction summand for transmission via path Dff

K_1 and K_2 depend on the slab, the screed applied and the flanking walls. The values are given in the adjacent table. K_2 is given as function of impact sound $L_{n,w} + K_1$.

- 1 gypsum fibreboard (GF) or plasterboard (GKB)
- 2 cross laminated timber (CLT) and GF or GKB (level of installation $d \geq 60\text{mm}$)
- 3 composite board
- 4 cross laminated timber (CLT)
- 5 LIGNATUR with suspended ceiling
- 6 LIGNATUR
- 7 wet screed on mineral fibre
- 8 dry screed on wood fibre



Example prognosis of vertical airborne and impact sound transmission



See the following demonstration for predicted values for your project in terms of airborne and impact sound transmission.

Basic conditions

$$l_{i,lab} = 4.5m, l_{b,lab} = 4.5m$$

$$l_{i,Bau} = 6.0m, l_{b,Bau} = 5.0m$$

$$A_0 = 10.0m^2, S_S = 30.0m^2$$

Floor system chosen

cement screed, mineral fibre insulation, bonded chippings, LIGNATUR silence12

$$R_w = 72dB$$

$$L_{n,w} = 44dB$$

Flanking elements example A

A_1, A_3 gypsum fibreboard (GF)

A_2, A_4 cross laminated timber and GF

- $R_{FF,w,R,1-4} = 72dB$

- $R_{Fd,w,R,1-4} = 70dB$

- $R_{Dd,w,R,1-4} \sim 85dB$

Prognosis example A

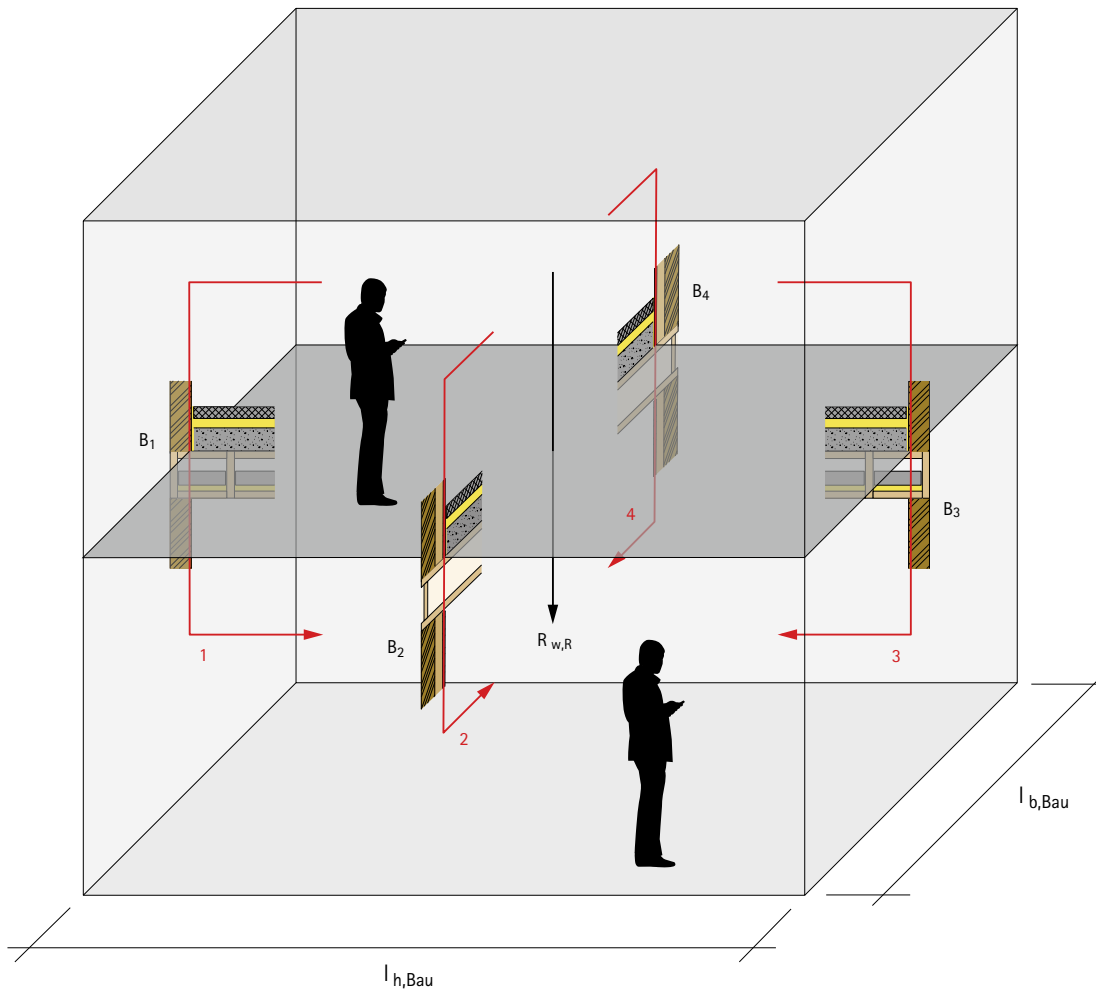
$$R'_w = 65dB$$

$$L'_{n,w} = 44dB + 1dB + 1 = 46dB$$

We are happy to predict the airborne and impact sound transmission for your project.



Example prognosis of vertical airborne and impact sound transmission



Basic conditions

$$l_{l,lab} = 4.5m, l_{b,lab} = 4.5m$$

$$l_{l,Bau} = 6.0m, l_{b,Bau} = 5.0m$$

$$A_0 = 10.0m^2, S_s = 30.0m^2$$

Floor system chosen

cement screed, mineral fibre insulation, bonded chippings, LIGNATUR silence12

$$R_w = 72dB$$

$$L'_{n,w} = 44dB$$

Flanking elements example B

B₁, B₃ cross laminated timber

- $R_{Ff,w,R,1+3} = 64dB$
- $R_{Fd,w,R,1+3} = 63dB$
- $R_{Dd,w,R,1+3} \sim 85dB$

B₂, B₄ cross laminated timber and GF

- $R_{Ff,w,R,2+4} = 72dB$
- $R_{Fd,w,R,2+4} = 70dB$
- $R_{Dd,w,R,2+4} \sim 85dB$

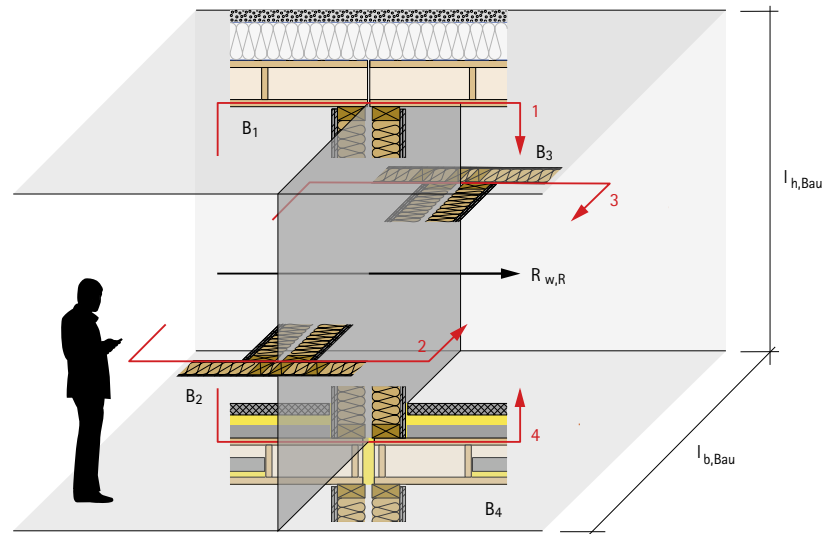
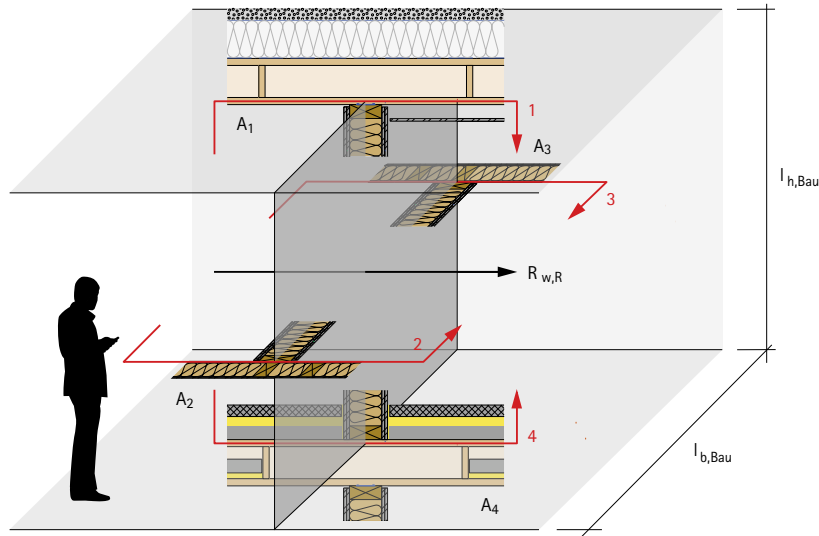
Prognosis example B

$$R'_w = 61dB$$

$$L'_{n,w} = 44dB + 4dB + 2 = 50dB$$



Example prognosis of horizontal airborne sound transmission



For support of this prognosis model for airborne sound insulation on horizontal levels on site, we have done various tests with the laboratory for building acoustics ift in Rosenheim. Two examples of prognoses from the research project are shown here.

Basic conditions

$$l_{b,lab} = 4.5m, l_{h,lab} = 2.8m$$

$$l_{b,Bau} = 6.0m, l_{h,Bau} = 2.8m$$

$$A_0 = 10.0m^2, S_S = 16.8m^2$$

Wall system chosen example A

2 · gypsum fibreboard (GF), timber frame (TF) construction insulated, 2 · GF
 $R_w = 46dB$

Side elements example A

- A₁ LIGNATUR, one-sided suspended ceiling, gravel roof
- $R_{Ff,w,R,1} = 53dB, R_{Fd,w,R,1} = 47dB, R_{Df,w,R,1} = 57dB$
- A₂, A₃ timber wall, panelling separated
- $R_{Ff,w,R,2-3} = 54dB, R_{Fd,w,R,2-3} = R_{Df,w,R,2-3} \approx 57dB$
- A₄ LIGNATUR silence12, screed
- $R_{Ff,w,R,4} = 70dB, R_{Fd,w,R,4} = R_{Df,w,R,4} = 80dB$

Prognosis example A

$$R'_w = 43dB$$

Wall system chosen example B

2 · gypsum fibreboard (GF), TF insulated, construction joint, TF insulated, 2 · GF
 $R_w = 65dB$

Side elements example B

- B₁ LIGNATUR separated, gravel roof
- $R_{Ff,w,R,1} = 62dB, R_{Fd,w,R,1} = R_{Df,w,R,1} > 70dB$
- B₂, B₃ timber wall, panelling separated
- $R_{Ff,w,R,2-3} = 68dB, R_{Fd,w,R,2-3} = R_{Dd,w,R,2-3} \approx 70dB$
- B₄ LIGNATUR silence12 separated, screed
- $R_{Ff,w,R,4} = 80dB, R_{Fd,w,R,4} = R_{Df,w,R,4} = 80dB$

Prognosis example B

$$R'_w = 59dB$$

We are happy to predict the airborne sound transmission for your project.